

Technical Memorandum

To: Mr. Patrick Jones Date: May 22, 2015

Project: High Plains Shooting Sports Center TIA

From: Omni-Means

Russell Wenham, PE, TE, PTOE

Kamesh Vedula, PE, TE

Re: Traffic Analysis for Proposed

High Plains Shooting Sports Center

Job No.: 45-5151-01

File No.: C1972MEM002.DOCX

CC:

Executive Summary

Omni-Means has performed a focused traffic impact analysis for the proposed High Plains Shooting Sports Center (hereafter referred to as the project) in the County of Shasta, CA. The analysis included calculating the number of vehicle trips generated by the project based on surveys of existing shooting ranges in the Shasta, Tehama, and Sacramento County areas. Vehicle trip rates from the surveys were derived from the linear footage of shooting space at the surveyed facilities and applied to the proposed project. The calculated project trips were added to existing weekday and weekend (Saturday) peak hour volumes surveyed at the project access intersection of Leopard Drive and Dersch Road. The traffic operations at the Leopard Drive/Dersch Road intersection were evaluated, including levels of service, vehicle queuing, and turn lane requirements. Traffic operating conditions were also analyzed for forecast Year 2035 volumes based on the Shasta County Regional Travel Demand Model. Sight distances were surveyed and compared to recommended sight distances established by the American Association of State Highway Transportation Officials guidelines.

Conclusions/Recommendations

- Level of service operating conditions for the Leopard Drive/Dersch Road intersection under existing and forecast Year 2035 conditions are acceptable without the project and would remain acceptable (LOS A) with the addition of the project trips.
- A vehicle queuing analysis was conducted for existing and forecast Year 2035 conditions.
 Queue lengths of 0-1 vehicles without the project would increase minimally, to 1-2 vehicles
 with the project during peak hours. Therefore, vehicle queues would be acceptable with the
 addition of the project trips.
- The intersection volumes were compared to peak hour signalization warrants to determine
 if the volumes would qualify for installation of a traffic signal. The volumes would not
 qualify for signalization under existing or future conditions without the project or with the
 added project trips.

- The intersection was evaluated for installation of separate turn lanes based on Caltrans
 design guidelines. Existing volumes and forecast Year 2035 volumes would remain below
 threshold levels without the project and with the addition of the project trips, therefore
 separate turn lanes are not warranted.
- The existing intersection sight distances (ISD) in both directions from Leopard Drive do not meet the recommended AASHTO distances due to existing vegetation and earth banks. This would be a <u>significant impact</u>.

To mitigate conditions with the project, it is recommended that the project applicant modify the earth banks by grading/excavation and controlling vegetation along the Leopard Drive and Dersch Road returns. Also, improvements to Leopard Drive, including asphalt pavement and shoulder backing at the connection to the Dersch Road intersection should be installed. Additional grading and clearing, if necessary, should be undertaken to achieve adequate sight distance. With these improvements, sight distances would be sufficient and extend beyond the recommended guidelines. This would mitigate the sight distance issue to a less than significant impact.

• Due to the nature of the project, that will attract many first-time or infrequent visitors, advance signing for Leopard Lane is recommended. The following signs will warn drivers that they are approaching Leopard Lane:

W2-2: T-Intersection Symbol

W16-8P: Supplemental Street Name Plaque



Introduction

This technical memorandum has been prepared by Omni-Means to present the results of a focused traffic impact analysis performed for the proposed High Plains Shooting Sports Center (hereafter referred to as the project) to be located on the east side of Leopard Drive north of Dersch Road in Shasta County, CA. The project, as referred to in this report, would consist of public skeet, trap, pistol, and long-rifle ranges with a 5,000 square foot clubhouse, and a separate law-enforcement range and clubhouse. The results of this analysis are intended for use in the project's environmental approval.

Included in this technical memorandum is analysis and discussion of the following items:

- Quantification of the trip generation and trip distribution associated with the proposed project.
- Identification of existing weekday and weekend peak hour intersection volumes and analysis of peak hour operations without the proposed project and with the project.
- The forecast Year 2035 peak hour intersection operating conditions without the project and with the project.
- Existing and projected safety conditions, including potential vehicle queue lengths, turn lane requirements, and sight distances at the Leopard Drive/Dersch Road intersection and in the project vicinity.
- Mitigation measures to alleviate substandard conditions at the study intersection.

The following traffic scenarios have been analyzed as a part of this technical memorandum:

- Existing Conditions
- Existing Plus Project Conditions
- Year 2035 No Project Conditions
- Year 2035 Plus Project Conditions

Existing conditions quantify the current traffic operations at the study locations.

The *Existing Plus Project* condition is an analysis scenario in which traffic impacts with the proposed project are investigated in comparison to the *Existing* conditions scenario. Within this scenario, the project generated peak hour volumes have been added to the *Existing* condition volumes to obtain the *Existing Plus Project* traffic volumes.

Year 2035 "No Project" conditions identify traffic operations based on cumulative forecast volumes derived from the Shasta County Travel Demand Model, minus the proposed project.

Year 2035 "Plus Project" conditions build upon Year 2035 "No Project" conditions by adding the project-generated trips to the forecast traffic volumes.

Existing Conditions

The proposed project would be located on the east side of Leopard Drive approximately one-half mile north of Dersch Road. The project vicinity and site location are shown in Figures 1 and 2, respectively. The roadways serving the project site are described as follows:

Leopard Drive is a rural, low-volume, dirt road extending north from Dersch Road for approximately one mile where it intersects with Impala Drive and Antler Road, which are also



low-volume dirt roads. The proposed project would be located along the eastern side of Leopard Drive beginning one-half mile north of Dersch Road and extend for one-half mile to Impala Drive. The entrance to the project site would be located at the southern project boundary one-half mile north of Dersch Drive. Leopard Drive enters a free-range cattle area after crossing a cattle-guard grate located approximately 200 feet north of Dersch Road. The surrounding landscape consists of range land with a few single-family homes and auxiliary buildings.

Dersch Road is oriented in a primarily east-west direction extending east from Airport Road in the City of Redding for approximately seven miles to Leopard Drive, then continues another four miles where it intersects with Ash Creek Road and curves north for four more miles to Route 44. Dersch Road is classified as a minor arterial in the California Department of Transportation roadway classification system. In the project vicinity, it is a rural two lane road with double-yellow centerline striping and white pavement edge striping. On each side of the paved road are unimproved shoulders with natural range land grass habitat. Dersch Road has a posted speed limit of 55 mph near Leopard Drive. The Dersch Road/Leopard Drive intersection is a T-intersection consisting of single lane approaches. Leopard Drive extends north from Dersch Road. There is a wide shoulder/turn-out area on the south side of Dersch Road at the Leopard Drive intersection location.

Existing Volumes

The project access intersection of Leopard Drive/Dersch Road was chosen for evaluation during Weekday PM and Weekend Afternoon peak periods of traffic flows. To identify existing volumes, vehicle counts were conducted at the study intersection by Omni-Means on a weekday from 4:00-6:00 pm and on a Saturday and Sunday from 11:00 am to 2:00 pm in order to identify the weekend day with the highest volumes. From these counts, the highest peak hour volumes were utilized for the traffic analysis. During the weekday peak hour, no vehicle trips were surveyed into or out of Leopard Drive and 106 trips were surveyed on Dersch Road. Weekend volumes were highest on Saturday, consisting of 2 trips on Leopard Drive and 86 trips on Dersch Road. The existing peak hour traffic volumes are shown in Figure 4.

Level-of-Service Methodologies

Traffic operations and impacts are typically quantified through the determination of "Level of Service" (LOS). Level of Service is a measure of traffic operating conditions, whereby a letter grade "A" through "F" is assigned to an intersection, representing progressively worsening traffic operations. LOS A represents free-flow conditions with little delay. LOS F represents congested conditions where traffic flows can exceed design capacities resulting in long vehicle queues and delays. At unsignalized intersections with minor-street stop control, stated LOS usually refers to the stop controlled approach with the highest delay and is expressed in seconds of delay. LOS criteria and definitions are provided in the Appendix. The peak hour intersection LOS calculations have been calculated based on the Transportation Research Board (TRB) publication *Highway Capacity Manual, Fourth Edition, 2000* (HCM-2000) methodology using Synchro/Simtraffic modeling software.² (Level-of-service calculation worksheets are provided in the Appendix.)

²Transportation Research Board (TRB), 2000 Highway Capacity Manual, Intersection Operations, Chapters 16 & 17.



¹ Omni-Means, Weekday AM (7:00-9:00 a.m.) and PM (4:00-6:00 p.m.) peak period intersection counts, May 5&7, 2015.

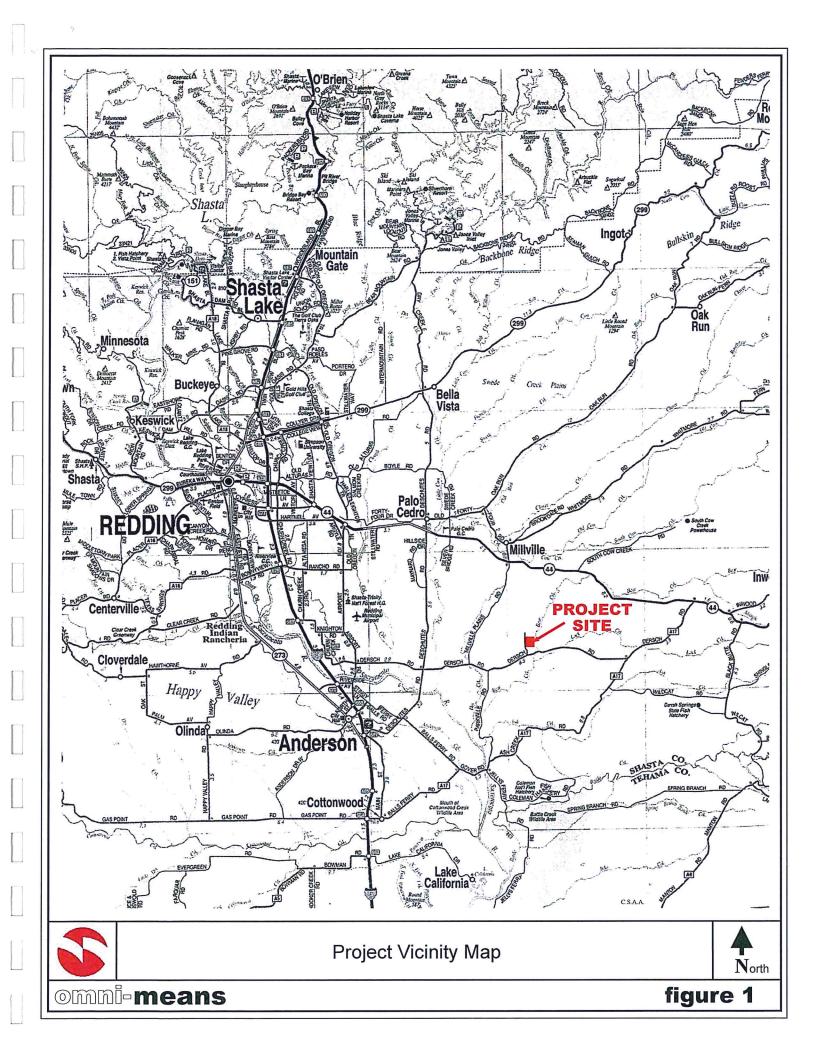




figure 2

Project Site Location



Level-of-Service Methodologies

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Significance Criteria

The following standards of significance have been used in this transportation analysis:

For two-way stop intersections, the project is considered to have a significant impact if:

- The project causes the following to occur for the worst-case movement:
 - The LOS declines to an unacceptable LOS, and
 - The volume to capacity ratio exceeds 0.75, and
 - The 95th percentile queue exceeds 75 feet (3 vehicles), OR
- The project causes the worst-case movement's acceptable LOS to decline to an unacceptable LOS and the peak hour volume signal warrant is met, OR
- The project increases the average delay for the worst-case movement by more than 5 seconds per vehicle at an intersection that has an unacceptable LOS without the project and the intersection also meets the peak hour volume signal warrant.

Existing Operating Conditions

A summary of the levels of service identified in this traffic analysis is provided in Table 2. As shown in Table 2, the Leopard Drive/Dersch Road intersection is operating at LOS A conditions on the weekday and weekend with minimal vehicle delays (8.8 seconds or less), which is representative of very efficient overall traffic flows.

Vehicular Queuing Analysis

A vehicle queuing analysis was conducted for existing conditions. Leopard Drive has calculated 95th percentile queue lengths of 11 feet or less, which equates to 0-1 vehicles (assuming 25 feet per vehicle). This corresponds with the observed queues of 0-1 cars during the counts. (Queuing calculation worksheets are provided in the Appendix.)

³Transportation Research Board (TRB), 2000 Highway Capacity Manual, Intersection Operations, Chapters 16 & 17.



Turn Lane Warrants

The intersection volumes were compared to Caltrans design guidelines regarding installation of separate turn lanes. For left turn lanes, peak hour traffic volumes are utilized by comparing the advancing and opposing volumes on Dersch Road with the percentage of left turning vehicles into the project access road.⁴ The volumes associated with the project conditions are well below the Caltrans minimum thresholds, therefore a left turn lane would not be warranted (left turn lane warrant graphs are provided in the Appendix).

The right turn volumes from Dersch Road are also well below minimum thresholds at which right turn lanes would be required (right turn lane warrant graphs are included in the Appendix.)⁵

Signal Warrants

To determine another level of "significance" associated with unsignalized intersection operations, a traffic signal "warrant" analysis has also been completed. The term "signal warrants" refers to established criteria used quantitatively to justify or ascertain the need for installation of a traffic signal at an otherwise unsignalized intersection location. This study employs the signal warrant criteria presented in the Manual on Uniform Traffic Control Devices (*California MUTCD*). Specifically, this study utilized the Peak Hour Warrant for the traffic signal analysis.

The peak hour signal warrant criteria were applied to the study intersection. The intersection volumes do not qualify for signalization under the peak hour criteria (signal warrant worksheets are provided in the Appendix).

Proposed Project

Project Description

The proposed project is a shooting facility that would consist of public skeet, trap, pistol, and long-rifle ranges with a 5,000 square foot clubhouse, and a separate law-enforcement range and clubhouse. The facility would provide approximately 1,500 linear feet of shooting positions encompassed within an approximately 140 acre parcel. The existing site consists of undeveloped range land. A project site plan is provided in Figure 3.

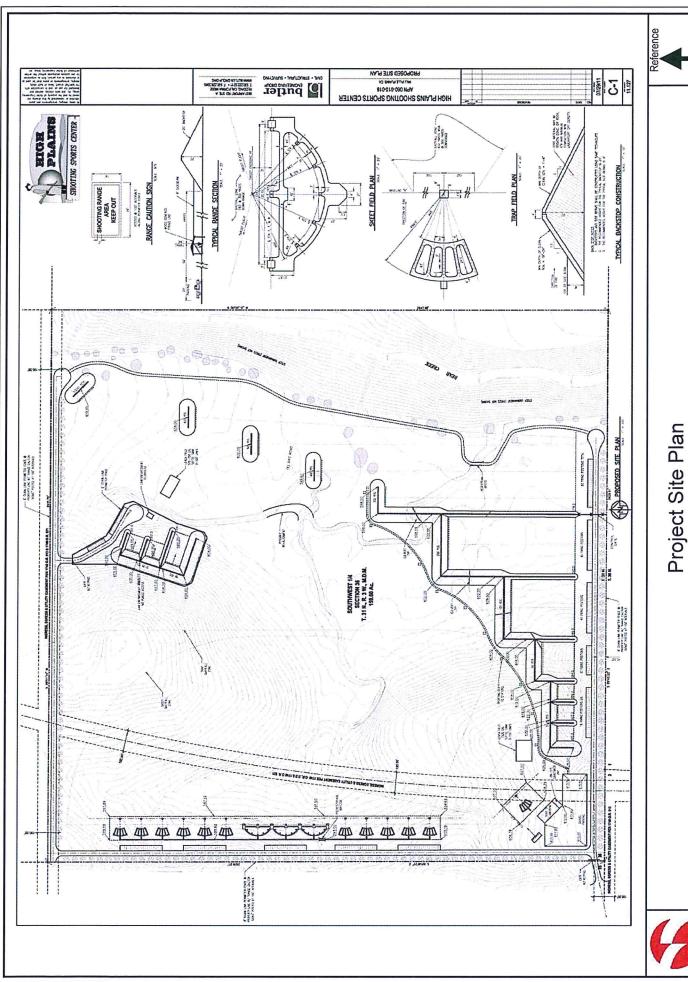
⁶ California Department of Transportation, <u>Manual on Uniform Traffic Control Devices</u>, 2014 Edition.



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⁴ California Department of Transportation, Guidelines for Reconstruction of Intersections, August 1985.

⁵ Transportation Research Board, National Cooperative Highway Research Program Report 279, "Intersection Channelization Design Guide", November 1985.



North figure 3

omni-means



Project Trip Generation

Vehicle trip generation for the proposed project was derived from surveys conducted by Omni-Means of existing shooting facilities within the greater Shasta, Tehama, and Sacramento County areas. (Published data for outdoor shooting facilities is limited and it is believed that surveys of local facilities will provide the most representative data.) For the study, five outdoor shooting clubs/venues were selected for evaluation. Four of the facilities are located in Shasta or Tehama County and share similar features with the proposed project, including locations in primarily rural areas. For comparison purposes, a fifth facility located in more densely populated Sacramento County was also surveyed. The following facilities were surveyed:

Shasta County/Tehama County:

Redding Gun Club

Shasta County Peace Officer Association (Record Range)

Hat Creek Rifle & Pistol Club

Tehama Shooters Association Gun Range

Sacramento County:

Sacramento Valley Shooting Center

Vehicle counts were conducted at the study facilities during a weekday PM period and during weekend Saturday and Sunday afternoon periods. Both weekend days were surveyed in order to identify the weekend day with the highest volumes. The surveyed weekend volumes were highest on Saturday. Based on the survey data, the highest peak hour volumes were utilized for the traffic analysis.

Trip rates were calculated for weekday and weekend peak hours by dividing the surveyed number of trips by the amount of linear feet provided for shooting positions at each facility. The surveyed number of trips and resulting trip generation rates are provided in Table 1.

The four locations with characteristics in common with the proposed project site (located in Shasta and Tehama Counties) shared similar trip rates. Weekday rates ranged from 0.01 to 0.02 trips per linear foot of shooting positions. The weekend Saturday rates ranged from 0.02 to 0.04 trips per linear foot of shooting positions. These facilities had an average trip rate of 0.02 weekday trips and 0.03 weekend trips per linear foot of shooting positions. The Sacramento Valley Shooting Center had higher trip rates of 0.06 weekday and 0.12 weekend trips per linear foot of shooting positions. These higher rates reflect the larger population base and limited number of facilities in the Sacramento region and are not reflective of the proposed location. The project could conceivably generate trips at such a rate on rare occasions, but these would be infrequent and would not constitute a basis for evaluation at a design level. Therefore, the trip rates from the four Shasta and Tehama County surveys were applied to the proposed project. As a conservative methodology, the *highest* observed trip rates (0.02 weekday and 0.04 weekend trips per linear foot of shooting positions) were utilized instead of the average rates to calculate the project trip generation.

The proposed project would consist of approximately 1,500 linear feet of shooting positions. Therefore, the proposed project was calculated to generate 30 weekday PM peak hour trips (12 in, 18 out) and 60 weekend peak hour trips (18 in, 42 out) as shown in Table 1.

⁷ Omni-Means, Weekday Counts conducted January 28, 29, and February 10, 2015. Weekend counts conducted February 14, 15, 21, 22, March 8, 28, and April 11, 2015.



Table 1: Summary of Surveyed Trip Rates For Existing Gun Ranges

			Surveyed Trips	
Tehama and Shasta Counties		Weekday	Saturday	Sunday
Shasta County Peace Officer Association Record Range 200 linear feet of shooting positions.	Peak Hour Volume: Time of Day: Peak Hour Trips per Linear Foot:	- (,,	4 (2 in, 2 out) 11:00 am - 12:00 pm 0.02	3 (2 in, 1 out) 12:00 - 1:00 pm 0.02
Redding Gun Club 575 linear feet of shooting positions.	Peak Hour Volume: Time of Day: Peak Hour Trips per Linear Foot:	4:00 - 5:00 pm	17 (3 in, 14 out) 12:30 - 1:30 pm 0.03	7 (0 in, 7 out) 1:00 - 2:00 pm 0.01
Hat Creek Rifle & Pistol Club 285 linear feet of shooting positions.	Peak Hour Volume: Time of Day: Peak Hour Trips per Linear Foot:	•	11 (3 in, 8 out) 11:30 am - 12:30 pm 0.04	No count: club says lower than Saturday. n.a.
Tehama Shooters Association Gun Range 405 linear feet of shooting positions.	Peak Hour Volume: Time of Day: Peak Hour Trips per Linear Foot:	8 (4 in, 4 out)* 4:00 - 5:00 pm 0.02	16 (5 in, 11 out) 11:30 am - 12:30 pm 0.04	No count: club says lower than Saturday. n.a.
Average Peak Hour Trips Per Linear Foot:		0.02 trips per l.f. (40% in, 60% out)	0.03 trips per l.f. (30% in, 70% out)	0.02 trips per l.f. 30% in, 70% out)
Highest Peak Hour Trips Per Linear Foot:		0.02 trips per l.f. (40% in, 60% out)	0.04 trips per l.f. (30% in, 70% out)	0.02 trips per l.f. 30% in, 70% out)

^{*}Based on average ratio of weekday to weekend peak hours. Club says typical trips likely lower.

PROJECT TRIP GENERATION

			Calculated Trips	
PROPOSED PROJECT (HIGH PLAINS SHOOTING CEN	TER) TRIP GENERATION	Weekday	Saturday	Sunday
1,500 linear feet of shooting positiions.	Peak Hour Trip Rate*: Peak Hour Volume:	• •	0.04 trips per l.f. = 60 (18 in, 42 out)	0.02 trips per l.f. = 30 (8 in, 22 out)

Project Trip Assignment

The project trips were distributed onto the street network based on the volume counts conducted for this study, the project's location relative to population areas, and the regional transportation facilities such as I-5 and Route 44. The turning movement counts indicate that directional distributions are different for the weekday and weekend peak periods. During the weekday pm period, a higher percentage of trips are to/from the west, which is most likely due to the proximity of the Redding population base. Based on these factors, the proposed project trips were assigned in the weekday pm with 65% to/from the west and 35% to/from the east. For



GEOMETRIES / CONTROLS: **PROJECT TRIPS** (21) 12 **4** (9) **4012** DERSCH RD. **PROJECT** SITE Weekday PM 30 (12 in, 18 out) Weekend Peak 60 (18 in, 42 out) DERSCH RD. EXISTING WITHOUT PROJECT **EXISTING PLUS PROJECT** PEAK HOUR VOLUMES: PEAK HOUR VOLUMES: (22) 0 (0) (9) 12 37 (43) 37 (43) DERSCH RD. DERSCH RD. 8 🛨 0 (0)(9)69 → (43)(43) 69 -



Existing And Existing Plus Project Weekday P.M. and (Weekend) Peak Hour Volumes



NOT TO SCALE

Cumulative Conditions

Cumulative Year 2035 Forecast Projections

Cumulative (Year 2035) volume projections on Dersch Road were derived from the Shasta County Regional Travel Demand Model (SCTDM) using the growth-increment method. The increase in volumes from the model's base year to year 2035 on Dersch Road is 30 PM peak hour trips. This equates to a 28% increase, representing an annual increase of 1.4 % per year for twenty years above the existing count volumes. The annual percentage increase was applied to the existing count volumes on Dersch Road. It is unlikely Leopard Drive would experience growth equal to Dersch Road. However, to remain conservative, it was assumed each turning movement to/from Leopard Drive without the project would consist of five (5) peak hour trips. The cumulative volumes are shown in Figure 5 and the LOS are shown in Table 2.

Cumulative Without Project Operating Conditions

Intersection conditions at the Leopard Drive/Dersch Road intersection were evaluated based on the cumulative volumes. Under cumulative without project conditions, the Leopard Drive southbound approach would operate at LOS A (9.2 seconds delay or better) during the weekday and weekend peak hours. The eastbound Dersch Road approach would operate at LOS A (delays less than one second) during both peak hours.

Cumulative Plus Project Operating Conditions

The project trips were added to the cumulative volumes. The Leopard Drive southbound approach would operate at LOS A (9.7 seconds delay or better) during the weekday and weekend peak hours. The eastbound Dersch Road approach would operate at LOS A (1.6 seconds delay or better) during both peak hours. Conditions would remain acceptable with the project trips.

Vehicular Queuing Analysis

Under cumulative without project conditions, the southbound Leopard Drive approach to Dersch Road has a calculated 95th percentile queue length of approximately 31 feet (1-2 cars) during the weekday and Saturday peak hours. With the added project trips, calculated queues are 48-55 feet, representing a 1 car increase. This increase would be acceptable. Eastbound queues on Dersch Road resulting from left turns onto Leopard Drive would remain 1 vehicle or less with the addition of the project trips.

Turn Lane Warrants

The cumulative volumes without the project and with the project would remain below the Caltrans thresholds for installation of a left turn lane or a right turn lane on Dersch Road.

Signal Warrants

Peak hour signal warrants were applied to the cumulative without project and cumulative with project volumes. The intersection would not qualify for signalization under the peak hour criteria.

Shasta Regional Transportation Agency, Shasta County Travel Demand Model, (ShastaSIM) adopted June 24, 2014..



TABLE 2
INTERSECTION IMPACT SUMMARY

		1/06/06/07/20/20	MARINE MARINE	roese (allega en estado estado esta		Seriest Contraction	951000000000000000000000000000000000000	area la composição	green articles of the control of
Leopard Drive / Dersch Road			EKDA	Y PM PE	AK HOUR	WEEKEND PEAK HOU			HOUR
Control Type: MSSC Target LOS: C		LOS	Delay	Pk. Hr. Signal Warrant	95 th % Queue Length	LOS	Delay	Pk. Hr. Signal Warrant	95 th % Queue Length
EXISTING	SB EB	A A	0.0 0.0	No	OK (0') OK (0')	A A	8.8 0.0	No	OK (18') OK (0')
EXISTING + PROJECT	SB EB	A A	9.0 0.8	No	OK (41') OK (0')	A A	9.3 1.3	No	OK (49') OK (3')
Increase Due To Project	SB EB		9.0 0.8				0.5 1.3		
Significant Impact?				No				No	
CUMULATIVE NO PROJECT	SB EB	A A	9.2 0.4	No	OK (33') OK (3')	A A	9.1 0.6	No	OK (33') OK (0')
CUMULATIVE + PROJECT	SB EB	A A	9.2 0.9	No	OK (44') OK (11')	A A	9.7 1.5	No	OK (53') OK (5')
Increase Due To Project	SB EB		0.0 0.5				0.6 0.9		
Significant Impact?				No	***************************************			No	

Legend: MSSC = Minor Street Stop Control; LOS = Level of Service; Delay is listed in "seconds per vehicle"; Queue Length is listed in feet.



GEOMETRIES / CONTROLS: **PROJECT TRIPS** (21) 12 **1** 4 (9) DERSCH RD. **STOP** DERSCH RD. **PROJECT** SITE Weekday PM 30 (12 in, 18 out) Weekend Peak 60 (18 in, 42 out) DERSCH RD. **CUMULATIVE WITHOUT PROJECT CUMULATIVE PLUS PROJECT** PEAK HOUR VOLUMES: PEAK HOUR VOLUMES: (2)5 (5) 9 (14) 47 (55) 47 (55) DERSCH RD. DERSCH RD. (14) 13 🗗 5 (5)(55) 89 -(55)89 →



Cumulative and Cumulative Plus Project Weekday P.M. and (Weekend) Peak Hour Volumes



NOT TO SCALE

VEHICULAR SIGHT DISTANCE EVALUATION

Design Speed for Dersch Road at Leopard Drive

The design speed is a selected speed used to determine the various geometric design features of a roadway. The selected design speed should consider the operating speed (observed free-flow vehicle speeds), topography, adjacent land use and the functional classification of the roadway. For the purposes of the analysis, the following design speed was identified as appropriate:

• 60 MPH Design Speed (55 MPH Speed Limit): Dersch Road at intersection of Leopard Drive.

Sight Distance Standards

The guidelines set forth in *A Policy on Geometric Design of Highways & Streets, 2011 Sixth Edition, AASHTO,* are appropriate for the setting. The American Association of State Highway and Transportation Officials (AASHTO) is a national organization that conducts research and establishes guidelines related to transportation facilities. The *Policy* is the most widely recognized set of guidelines for local street design parameters.

Sight distance is the length of the roadway ahead that is visible to the driver. The available sight distance on a roadway should be sufficiently long to enable a vehicle traveling at or near the design speed to stop before reaching a stationary object in its path.

There are two sight distance standards that were selected for this analysis:

Stopping Sight Distance (SSD). SSD is the sum of two distances; (1) the distance traversed by the vehicle from the instant that driver sights an object necessitating a stop to the instant the brakes are applied, and (2) the distance needed to stop the vehicle from the instant brake application begins. These are referred to as brake reaction distance and braking distance, respectively.

SSD assumes a driver's eye height of 3.5 feet above the road on the approaching vehicle and a 2.0 feet high object stopped in the roadway. The SSD value that will be used for the analysis is:

60 MPH Design Speed: 570 LF

The recommended stopping sight distance is based on passenger car operation and does not explicitly consider truck operations. Trucks as a whole, especially the larger and heavier trucks, need longer stopping distances for a given speed than passenger vehicles. However, there is one factor that offsets the additional braking lengths for trucks. The truck driver is able to see substantially farther beyond vertical sight obstructions because of the higher position of the driver's eye (usually in excess of 7.5 feet). Simply put, if there is adequate SSD for an automobile, there is adequate SSD for trucks.

Intersection Sight Distance (ISD). In addition to SSD, sight distance is also needed at the project intersection to allow drivers of vehicles waiting to pull out of a driveway a sufficient view of Dersch Road to decide when to pull out on to Dersch Road. ISD assumes a driver's eye height of 3.5 feet above the driveway and the approaching



vehicle to be seen is 3.5 feet above the roadway on Dersch Road. There are two cases that need to be considered; Left Turn from Leopard Drive and Right Turn from Leopard Drive. In both cases, the following standards apply:

- The vertex (decision point) of the vehicle in a driveway is 15 feet from the edge of traveled way for Leopard Drive. The time gap needed for this turning maneuver is 7.5 seconds for passenger vehicles.
- The ISD for the selected design speed is as follows:
 - o 60 MPH Design Speed: 665 LF from decision point.

Dersch Road at Leopard Drive

The SSD was measured by Omni-Means at each observed obstruction in both the eastbound and westbound directions of the intersection. The SSD measurements are shown in Table 3.

Table 3
Dersch Road Sight Distances

Location	SSD Guideline	Measured SSD
Leopard Drive	570 LF	800 LF

Notes: Field measurements considered accurate to +/-10%.

Existing Leopard Drive

The ISD was measured 15 feet from the edge of traveled way for Leopard Drive and is presented in Table 4.

Table 4
Intersection Sight Distances – Leopard Drive

£	intersection digite bis	ances - Leopard Drive	
ISD Guideline	Measured ISD: Easterly of the driveway (Approaching from the west)	Measured ISD: Westerly of the driveway (Approaching from the east)	ISD Limiting Condition
665 LF	-	120 LF	Vegetation and Earth Banks
665 LF	105 LF	-	Vegetation and Earth Banks

Notes: (1) Field measurements considered accurate to +/-10%.

(2) **Bold** = less than guideline.



As noted in Table 4, the Intersection Sight Distances at the existing Leopard Drive intersection do not meet AASHTO guidelines. Both the easterly and westerly approach ISD are restricted by the existing vegetation and earth banks.

Intersection Sight Distance Related Mitigation Measures

CEQA standards are not available to identify at what point sight distance issues are significant. Since project's are required to mitigate their significant impacts, traffic engineering judgment is required to identify at what point mitigation is required and to what extent.

To mitigate the project's impacts, it is recommended that the intersection sight distance restrictions that are created by vegetation and earth banks be modified so that the AASHTO guideline values can be achieved. It is recommended that both banks are excavated along the existing Leopard Drive and Dersch Road returns, and that vegetation is controlled at both returns. Improvements to Leopard Drive, including asphalt pavement and shoulder backing, may provide the guideline sight distance, but additional grading and clearing may be required to fully achieve the necessary sight distance. Fixing these restrictions will allow for an extended line of sight well beyond the current ISD conditions at this intersection and will provide sufficient distance to meet the AASHTO guidelines.



APPENDIX

High Plains Shooting Sports Center TIA

Surveyed Trip Rates of Existing Gun Ranges

Level of Service Definitions

LOS Calculation Worksheets

Vehicle Queuing Worksheets

Turn Lane Warrant Worksheets

Signal Warrant Worksheets



SURVEYED TRIP RATES OF EXISTING GUN RANGES

Tehama and Shasta Counties		West 1	Surveyed Trips		
Tenama and Shasta Counties		Weekday	Saturday	Sunday	
Shasta County Peace Officer Association Record Range 200 linear feet of shooting positions.	Peak Hour Volume: Time of Day: Peak Hour Trips per Linear Foot:	3 (1 in, 2 out) 4:15 - 5:15 pm 0.02	4 (2 in, 2 out) 11:00 am - 12:00 pm 0.02	3 (2 in, 1 out) 12:00 - 1:00 pm 0.02	
	Total Survey Volume: Time of Day: Average Hourly Trips per Linear Foot:	3 (1 in, 2 out) 4:00 - 6:00 pm 0.01	7 (3 in, 4 out) 11:00 am - 2:00 pm 0.01	5 (3 in, 2 out) 11:00 am - 2:00 pm 0.01	
Redding Gun Club 575 linear feet of shooting positions.	Peak Hour Volume: Time of Day: Peak Hour Trips per Linear Foot:	4 (2 in, 2 out) 4:00 - 5:00 pm 0.01	17 (3 in, 14 out) 12:30 - 1:30 pm 0.03	7 (0 in, 7 out) 1:00 - 2:00 pm 0.01	
373 inteat feet of shooting positions.	Total Survey Volume: Time of Day: Average Hourly Trips per Linear Foot: Notes:	8 (3 in, 5 out) 4:00 - 6:00 pm 0.01	37 (13 in, 24 out) 11:00 am - 2:00 pm 0.02 U.S.P.S.A. Match	12 (1 in, 11 out) 11:00 am - 2:00 pm 0.01 Hours 9am - 3pm	
Hat Creek Rifle & Pistol Club 285 linear feet of shooting positions.	Peak Hour Volume: Time of Day: Peak Hour Trips per Linear Foot:	5 (2 in, 3 out)* 4:00 - 5:00 pm 0.02	11 (3 in, 8 out) 11:30 am - 12:30 pm 0.04	No count: club says lower than Saturday. n.a.	
	Total Survey Volume: Time of Day: Average Hourly Trips per Linear Foot:	*Based on ratio of wkday. to wkend. peak hours.	17 (4 in, 13 out) 11:00 am - 1:00 pm 0.03	No count: club says lower than Saturday. n.a.	
Tehama Shooters Association Gun Range	Peak Hour Volume: Time of Day:	8 (4 in, 4 out)* 4:00 - 5:00 pm	16 (5 in, 11 out) 11:30 am - 12:30 pm	No count: club says lower than Saturday.	
405 linear feet of shooting positions.	Peak Hour Trips per Linear Foot: Total Survey Volume: Time of Day: Average Hourly Trips per Linear Foot: Notes:	*Based on ratio of wkday. to wkend. peak hours.	0.04 24 (6 in, 18 out) 11:00 am - 1:00 pm 0.03 Rifle & handgun competition.	n.a. No count: club says lower than Saturday. n.a.	
Average Peak Hour Trips Per Linear Foot:		0.02 trips per l.f. (40% in, 60% out)	0.03 trips per l.f. (30% in, 70% out)	0.02 trips per l.f. 30% in, 70% out)	
Highest Peak Hour Trips Per Linear Foot:		0.02 trips per l.f. (40% in, 60% out)	0.04 trips per l.f. (30% in, 70% out)	0.02 trips per l.f. 30% in, 70% out)	

			Calculated Trips	
PROPOSED PROJECT (HIGH PLAINS SHOOTING CEN	NTER) TRIP GENERATION	Weekday	Saturday	Sunday
1,500 linear feet of shooting positiions.	Peak Hour Trip Rate: Peak Hour Volume:		0.04 trips per l.f. = 60 (18 in, 42 out)	0.02 trips per l.f. = 30 (8 in, 22 out)
		Based on highest ob	served trip rates to remain	n conservative.

SURVEYED TRIP RATES OF EXISTING GUN RANGES

			Surveyed Trips	
Sacramento County		Weekday	Saturday	Sunday
Sacramento Valley Shooting Center	Peak Hour Volume:	29 (0 in, 29 out)	68 (16 in, 52 out)	64 (17 in, 47 out)
470 linear feet of shooting positions	Time of Day: Peak Hour Trips per Linear Foot:		11:45 am - 12:45 pm 0.14	12:15 - 1:15 pm 0.14
	Total Survey Volume: Time of Day: Average Hourly Trips per Linear Foot:	•	174 (49 in, 125 out) 11:00 am - 2:00 pm 0.12	165 (58 in, 107 out) 11:00 am - 2:00 pm 0.12

LEVEL-OF-SERVICE CRITERIA FOR INTERSECTIONS

		LEVEL-OF-SERVICE C	SVEL-OF-SERVICE CRITERIA FOR INTERSECTIONS	,		
LEVEL OF				CONTRO	CONTROL DELAY (SECONDS/VEHICLE)	EHICLE)
SERVICE	TYPE OF FLOW	DELAY	MANEUVERABILITY	SIGNALIZED	Unsignalized	ALL-WAY STOP
γ	Stable Flow	Very slight delay. Progression is very favorable, with most vehicles arriving during the green phase not stopping at all.	Turning movements are easily made, and nearly all drivers find freedom of operation.	≤ 10.0 secs. ≤ 0.60 v/c	≥ 10.0	∨ 100
B	Stable Flow	Good progression and/or short cycle lengths. More vehicles stop than for LOS A, causing higher levels of average delay.	Vehicle platoons are formed. Many drivers begin to feel somewhat restricted within groups of vehicles.	>10 and \leq 20.0 secs. 0.61 - 0.70 v/c	>10 and ≤ 15.0	>10 and ≤ 15.0
O	Stable Flow	Higher delays resulting from fair progression and/or longer cycle lengths. Individual cycle failures may begin to appear at this level. The number of vehicles stopping is significant, although many still pass through the intersection without stopping.	Back-ups may develop behind turning vehicles. Most drivers feel somewhat restricted	>20 and ≤ 35.0 secs. 0.71 – 0.80 v/c	>15 and ≤ 25.0	>15 and ≤ 25.0
Q	Approaching Unstable Flow	The influence of congestion becomes more noticeable. Longer delays may result from some combination of unfavorable progression, long cycle lengths, or high volume-to-capacity ratios. Many vehicles stop, and the proportion of vehicles of stopping declines. Individual cycle failures are noticeable.	Maneuverability is severely limited during short periods due to temporary back-ups.	>35 and ≤ 55.0 secs. 0.81 – 0.90 v/c	>25 and ≤ 35.0	>25 and ≤ 35.0
E	Unstable Flow	Generally considered to be the limit of acceptable delay. Indicative of poor progression, long cycle lengths, and high volume-to-capacity ratios. Individual cycle failures are frequent occurrences.	There are typically long queues of vehicles waiting upstream of the intersection.	>55 and ≤ 80.0 secs. 0.91 – 1.00 v/c	>35 and ≤ 50.0	>35 and ≤ 50.0
	Forced Flow	Generally considered to be unacceptable to most drivers. Often occurs with over saturation. May also occur at high volume-to-capacity ratios. There are many individual cycle failures. Poor progression and long cycle lengths may also be major contributing factors.	Jammed conditions. Back-ups from other locations restrict or prevent movement. Volumes may vary widely, depending principally on the downstream back-up conditions.	> 80.0 secs.	> 50.0	> 50.0
) C					Transport Control Cont	

Reference: Transportation Research Board, Highway Capacity Manual 2010.

Intersection									
Intersection Delay, s/veh	0								
Movement	EBL	EBT			WBT	WBR	SBL	SBR	
Vol, veh/h	0	69			37	0	0	0	
Conflicting Peds, #/hr	0	0			0	0	0	0	
Sign Control	Free	Free			Free	Free	Stop	Stop	
RT Channelized	None	None			None	None	None	None	
Storage Length	0					0	0	0	
Median Width		0			0		12		
Grade, %		0%			0%		0%		
Peak Hour Factor	0.78	0.78			0.66	0.66	1.00	1.00	
Heavy Vehicles, %	2	2			2	2	2	2	
Mymt Flow	0	88			56	0	0	0	
Number of Lanes	0	1			1	0	1	0	
Major/Minor		Major 1		823800758	Major 2				
Conflicting Flow All	56	0	10 - 0 1 - 1		_	0	144	56	
Stage 1	- 00						56	-	
Stage 2		h (nasqipta			- Eschige		88		
Follow-up Headway	2.218	s. Individues.			Janes J. E.G.	del allakon	3.518	3.318	
Pot Capacity-1 Maneuver	1549	E ENTRAFE			ann dia si	3073	849	1011	
	1049				art or subtra	in and a second	967	1011	
Stage 1							935		
Stage 2	0						0	0	
Time blocked-Platoon, %							849	1011	
Mov Capacity-1 Maneuver	1549	an sue avillacen			€ Unicatisa wa£	rzenia najliwawa	849	1011	
Mov Capacity-2 Maneuver					•				
Stage 1	rens refereibet	and containing			· Santida en San		967	May a Samuel et an inflavori	
Stage 2		•			•		935	•	
Approach	EB				WB		SB		
HCM Control Delay, s	0				0		0		
HCM LOS	•						Α		
Minor Lane / Major Mvmt		EBL	EBT	WBT	WBR	SBLn1			
Cap, veh/h		1549	0.51	-	-	0			171
HCM Control Delay, s		0	2	1		0			
HCM Lane V/C Ratio			s: 11.50±***5##\$\$\.i	-	_	-			
HCM Lane LOS		Α				Α			
HCM 95th-tile Q, veh		0.0	autor a sustant		- 				
Notes		0.0							**********

^{~:} Volume Exceeds Capacity; \$: Delay Exceeds 300 Seconds; Error: Computation Not Defined

Intersection	0.3								
ntersection Delay, s/veh	0.3								
Movement	EBL	EBT			WBT	WBR	SBL	SBR	
Vol, veh/h	0	43		e vez evez	43	0	1	1	TO THE STATE OF THE PARTY.
Conflicting Peds, #/hr	0	0			0	0	0	0	
Sign Control	Free	Free			Free	Free	Stop	Stop	
RT Channelized	None	None			None	None	None	None	
Storage Length	0					0	0	0	
Median Width		0			0		12		
Grade, %		0%			0%		0%		
Peak Hour Factor	0.67	0.67			0.90	0.90	0.50	0.50	
Heavy Vehicles, %	2	2			2	2	2	2	
Mymt Flow	0	64			48	0	2	2	
Number of Lanes	0	1			1	0	1	0	
Number of Lanes	U	A SHOULD A				U		U	
Major/Minor		Major 1			Major 2				
Conflicting Flow All	48	0			-	0	112	48	
Stage 1	-						48		
Stage 2		-			-		64	-	
Follow-up Headway	2.218					•	3.518	3.318	
Pot Capacity-1 Maneuver	1559	-				-	885	1021	
Stage 1						in the state of	974		
Stage 2					5	· · · · · · · · · · · · · · · · · · ·	959	a no se se je nasjenjenska :	
Time blocked-Platoon, %	0						0	0	
Mov Capacity-1 Maneuver	1559	Litera x sistenim			o modifica	answeight and	885	1021	
Mov Capacity-2 Maneuver	1000						885		
Stage 1		Maria Maria					974		
						ing keyesinkani	959		
Stage 2						•	505		
Approach	EB				WB		SB		
HCM Control Delay, s	0		-		0		8.8		
HCM LOS	-				•		Α		
Minor Lane / Major Mvmt		EBL	EBT	WBT	WBR	SBLn1			
			LOI	VVDI	VVDI				
Cap, veh/h		1559	e de la companie de l	e marko a seebaa		948			
HCM Control Delay, s		0	•	•	•	8.8			
HCM Lane V/C Ratio		ie.		a paragraphic di sa	market with	0.00			
HCM Lane LOS		Α	10	•	•	Α			
HCM 95th-tile Q, veh		0.0	•	-	-	0.0			

^{~:} Volume Exceeds Capacity; \$: Delay Exceeds 300 Seconds; Error: Computation Not Defined

Intersection									
Intersection Delay, s/veh	2								
Movement	EBL	EBT			WBT	WBR	SBL	SBR	
Vol, veh/h	8	69			37	4	6	12	
Conflicting Peds, #/hr	3	0			0	3	0	0	
Sign Control	Free	Free			Free	Free	Stop	Stop	
RT Channelized	None	None			None	None	None	None	
Storage Length	0	110110			140110	0	0	0	
Median Width		0			0		12	on to the amount of control of the same	
Grade, %		0%			0%		0%		
Peak Hour Factor	0.78	0.78			0.66	0.66	0.50	0.50	
Heavy Vehicles, %	2	2			2	2	2	2	
Mymt Flow	10	88			56	6	12	24	
Number of Lanes	0	1			1	0	1	0	
Number of Lanes	U				1	U	l	•	
Major/Minor		Major 1			Major 2				
Conflicting Flow All	62	0			-	0	168	62	
Stage 1	70,000					•	59		
Stage 2		-			-	-	109	•	
Follow-up Headway	2.218	i Bari					3.518	3.318	
Pot Capacity-1 Maneuver	1541	-			-	-	822	1003	
Stage 1	•				•		964		
Stage 2		-			-	-	916		
Time blocked-Platoon, %	0	-				•	0	0	
Mov Capacity-1 Maneuver	1537						816	1000	
Mov Capacity-2 Maneuver					i i	•	816		
Stage 1	-	·			-	-	964	-	
Stage 2	Y	100			•	•	910		
Approach	EB			0.52000000	WB		SB		
	0.8		Marie Colonia		0		9		
HCM Control Delay, s	0.8				U		9 A		
HCM LOS							А		
Minor Lane / Major Mvmt		EBL	EBT	WBT	WBR	SBLn1			
Cap, veh/h		1537	-			930			
HCM Control Delay, s		7.358	0		•	9			
HCM Lane V/C Ratio		0.01	-	•		0.04			
HCM Lane LOS		Α	Α	-		Α			
HCM 95th-tile Q, veh		0.0	-			0.1			
Notes							STEER ETASIS		

^{~:} Volume Exceeds Capacity; \$: Delay Exceeds 300 Seconds; Error: Computation Not Defined

Intersection										
Intersection Delay, s/veh	4.1									
Movement	EBL	EBT			WBT	WBR	SBL	SBR		
Vol, veh/h	9	43			43	9	22	22		
Conflicting Peds, #/hr	3	0			0	3	0	0		
Sign Control	Free	Free			Free	Free	Stop	Stop		
RT Channelized	None	None			None	None	None	None		
Storage Length	0					0	0	0		
Median Width	remaining page and	0			0		12			
Grade, %		0%			0%		0%			
Peak Hour Factor	0.67	0.67			0.90	0.90	0.50	0.50		
Heavy Vehicles, %	2	2			2	2	2	2		
Mymt Flow	13	64			48	10	44	44		
Number of Lanes	0	1			1	0	1	0		
Major/Minor		Major 1			Major 2					
Conflicting Flow All	58	0			-	0	144	56		8-22-20E
Stage 1	JU	U			ATTENDO	_	53			
Stage 2	•	Service of the Control of the Contro			_		91	•		
Follow-up Headway	2.218	e www.bisterliensa			alaba at A <u>l</u> ija		3.518	3.318		
Pot Capacity-1 Maneuver	1546	of Languages in				LANCE CONTROL	849	1011	MANAGEMENT OF THE PARTY OF THE	
Stage 1	1340	enda a 2000 de				240.32	970			
Stage 2							933	·		
Time blocked-Platoon, %	0	Kranis (1954)			maran <u>.</u>	in car	0	0		
Mov Capacity-1 Maneuver	1542	Mr. M.			Manual Pro-		841	1008		
Mov Capacity-2 Maneuver	1042				en su <u>.</u>	DANSE.	841	1000		
Stage 1							970			
Stage 2							925	•		
					WD		60			MEE'N
Approach	EB				WB		SB	Established Institute		
HCM Control Delay, s	1.3				0		9.3			
HCM LOS	•						Α			
Minor Lane / Major Mvmt		EBL	EBT	WBT	WBR	SBLn1				
Cap, veh/h		1542		•	-	917				
HCM Control Delay, s		7.355	0	•	•	9.3				
HCM Lane V/C Ratio		0.01	-	-	-	0.10				
HCM Lane LOS		Α	Α	-		Α				
HCM 95th-tile Q, veh		0.0	-	-	-	0.3				
Notes										

^{~:} Volume Exceeds Capacity; \$: Delay Exceeds 300 Seconds; Error: Computation Not Defined

Intersection Delay, s/veh	0.7								
Movement	EBL	EBT			WBT	WBR	SBL	SBR	
Vol, veh/h	5	89			47	5	5	5	
Conflicting Peds, #/hr	0	0			0	0	0	0	
Sign Control	Free	Free			Free	Free	Stop	Stop	
RT Channelized	None	None			None	None	None	None	
Storage Length	0					0	0	0	
Median Width		0			0		12	2 mm/1 1999 (19 mm/1 19 mm/2) (1996 (1997) (1997)	
Grade, %		0%			0%		0%		
Peak Hour Factor	0.78	0.78			0.66	0.66	1.00	1.00	
Heavy Vehicles, %	2	2			2	2	2	2	
Mymt Flow	6	114			71	8	5	5	
Number of Lanes	0	1			1	0	1	0	
Major/Minor		Major 1			Major 2				
Conflicting Flow All	79	0			-	0	202	75	AND DESCRIPTION OF THE OWNER, WHEN
Stage 1					-		75	gerendy internalial este	
Stage 2	with the settings				-	-	127		
Follow-up Headway	2.218				-		3.518	3.318	
Pot Capacity-1 Maneuver	1519	-			-		787	986	
Stage 1						1216.5025	948		
Stage 2	-				-	- 11700 117 117 117 117 117 117 117 117 1	899		
Time blocked-Platoon, %	0	100					0	0	
Mov Capacity-1 Maneuver	1519	-			Friedrich anders	-	784	986	
Mov Capacity-2 Maneuver		<u> </u>				in The	784	MATERIAL PROPERTY.	
Stage 1	-	-			-		948		
Stage 2	•	for each					895		
Approach	EB				WB		SB		
HCM Control Delay, s	0.4				0		9.2		
HCM LOS					·		A		
Minor Lane / Major Mvmt		EBL	EBT	WBT	WBR	SBLn1			
Cap, veh/h		1519	_	-	-	873			
HCM Control Delay, s		7.38	0			9.2			
HCM Lane V/C Ratio		0.00	And the state of t	Fellich mangle A.	-	0.01			
HCM Lane LOS		Α	A			Α.			
HCM 95th-tile Q, veh		0.0	-	agog negative 7000	processor (150) •	0.0			
		3.0				0.0			

^{~:} Volume Exceeds Capacity; \$: Delay Exceeds 300 Seconds; Error : Computation Not Defined

Intersection	4.0								
Intersection Delay, s/veh	1.3								
Movement	EBL	EBT			WBT	WBR	SBL	SBR	
Vol, veh/h	5	55			55	5	5	5	
Conflicting Peds, #/hr	0	0			0	0	0	0	
Sign Control	Free	Free			Free	Free	Stop	Stop	
RT Channelized	None	None			None	None	None	None	
Storage Length	0					0	0	0	
Median Width		0			0		12		
Grade, %		0%			0%		0%		
Peak Hour Factor	0.67	0.67			0.90	0.90	0.50	0.50	
Heavy Vehicles, %	2	2			2	2	2	2	
Mymt Flow	7	82			61	6	10	10	
Number of Lanes	ó	1			1	Ö	1	0	
Number of Lanes	U	14. € .50			10. 76.555 1 5	U		U	
Major/Minor		Major 1			Major 2				
Conflicting Flow All	67	0				0	161	64	
Stage 1							64		
Stage 2	•	<u>~</u>			•	-	97	·	
Follow-up Headway	2.218	•				•	3.518	3.318	
Pot Capacity-1 Maneuver	1535	-			-	-	830	1000	
Stage 1		<u></u>			- 1111		959		
Stage 2	Trans and reserve	Alberta Case III			-		927	TO STACING THE SHARE ANGEN	
Time blocked-Platoon, %	0	arteliting.					0	0	
Mov Capacity-1 Maneuver	1535	- AC-11 (AC-12)			-	Acres conties	826	1000	
Mov Capacity-2 Maneuver							826		
Stage 1		_			5.00		959		
Stage 2	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1				- -	teikade en Literatura	922		
Approach	EB				WB		SB		
HCM Control Delay, s	0.6				0		9.1		
HCM LOS	•				•		Α		
Minor Lane / Major Mymt		EBL	EBT	WBT	WBR	SBLn1			
Cap, veh/h		1535		_		905			
HCM Control Delay, s		7.357	0	45 6 6 <u>-</u>		9.1			
HCM Lane V/C Ratio		0.01	-		waren ja	0.02			
HCM Lane LOS		0.01 A	A	- Walley San	eriye ku	0.02 A			
HCM 95th-tile Q, veh		0.0	А	SAME O		0.1			
TOW Sour-life Q, Vell		0.0	•	-		0.1			

Intersection									
ntersection Delay, s/veh	1.5								
Movement	EBL	EBT			WBT	WBR	SBL	SBR	
Vol, veh/h	13	89			47	9	11	17	
Conflicting Peds, #/hr	0	0			0	0	0	0	
Sign Control	Free	Free			Free	Free	Stop	Stop	
RT Channelized	None	None			None	None	None	None	
Storage Length	0					0	0	0	
Median Width		0			0		12	Taran Terangangan Terang Sedica Se	
Grade, %		0%			0%		0%		
Peak Hour Factor	0.78	0.78			0.66	0.66	1.00	1.00	
Heavy Vehicles, %	2	2			2	2	2	2	
Mymt Flow	17	114			71	14	11	17	
Number of Lanes	0	114			1	0	1	0	
Tambor of Editor	•					•			
Major/Minor		Major 1			Major 2				
Conflicting Flow All	85	0			-	0	225	78	
Stage 1	-	•					78		
Stage 2		-			-		147		
Follow-up Headway	2.218	- n <u>-</u>				•	3.518	3.318	
Pot Capacity-1 Maneuver	1512				-		763	983	
Stage 1							945		
Stage 2	•	-			-	• • • • • • • • • • • • • • • • • • •	880		
Time blocked-Platoon, %	0	_			4.30.044	100 Maria	0	0	
Mov Capacity-1 Maneuver	1512	-			-	•	754	983	
Mov Capacity-2 Maneuver					•	•	754		
Stage 1		renew to be stated on			and The Manager		945		
Stage 2	Tarin ar	<u>.</u>			raines, i <u>e</u> r	er er er er	869	eliterativa <u>.</u>	
							000		
Approach	EB				WB		SB		
HCM Control Delay, s	0.9				0		9.2		
HCM LOS	•				-		Α		
Minor Lane / Major Mvmt		EBL	EBT	WBT	WBR	SBLn1			
Cap, veh/h		1512		NAD!	YVUN				
			-	elita antivanima	gios el Visio	878			
ICM Lors V/C Datie		7.407	0	100		9.2			
ICM Lane V/C Ratio		0.01	-	er Santhariel	-	0.03			
ICM Lane LOS		Α	Α	•	•	Α			
ICM 95th-tile Q, veh		0.0	-	-	-	0.1			
lotes									10.00

Intersection									
Intersection Delay, s/veh	4.1		Wallet 1220	v selection of					
Movement	EBL	EBT			WBT	WBR	SBL.	SBR	
Vol, veh/h	14	55			55	14	26	26	
Conflicting Peds, #/hr	0	0			0	0	0	0	
Sign Control	Free	Free			Free	Free	Stop	Stop	
RT Channelized	None	None			None	None	None	None	
Storage Length	0					0	0	0	
Median Width		0			0		12		
Grade, %		0%			0%		0%		
Peak Hour Factor	0.67	0.67			0.90	0.90	0.50	0.50	
Heavy Vehicles, %	2	2			2	2	2	2	
Mymt Flow	21	82			61	16	52	52	
Number of Lanes	0	1			1	0	1	0	
Major/Minor		Major 1			Major 2				
Conflicting Flow All	77	0			-	0	193	69	
Stage 1		•				•	69	•	
Stage 2	-	-			•	-	124	•	
Follow-up Headway	2.218					1.	3.518	3.318	
Pot Capacity-1 Maneuver	1522	-			-	-	796	994	
Stage 1	•					•	954		
Stage 2		-			-	-	902	-	
Time blocked-Platoon, %	0				•	1.00	0	0	
Mov Capacity-1 Maneuver	1522	•			•	-	785	994	
Mov Capacity-2 Maneuver						and the state of	785		
Stage 1	-	-				ALLONG HOLLENGER	954	en en la	
Stage 2	in .	-				i i	889	•	
A	ED	STATE STATE OF THE			WD		OD		
Approach	EB				WB		SB		
HCM Control Delay, s	1.5				0		9.7		
HCM LOS	0.3/2				•		Α		
Minor Lane / Major Mvmt		EBL	EBT	WBT	WBR	SBLn1			
Cap, veh/h		1522	-	-		877			
HCM Control Delay, s		7.398	0		-	9.7			
HCM Lane V/C Ratio		0.01	-		**************************************	0.12			
HCM Lane LOS		Α	Α	- 1	-	A			
HCM 95th-tile Q, veh		0.0		•	-	0.4			
Notes									

~: Volume Exceeds Capacity; \$: Delay Exceeds 300 Seconds; Error : Computation Not Defined

Queuing	and	Blocking	Report	
	•	. = .		

Existing Weekday PM Peak Hour

Directions Served	
Maximum Queue (ft)	
Average Queue (ft)	
95th Queue (ft)	
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Movement	SB	
Directions Served	LR	
Maximum Queue (ft)	31	
Average Queue (ft)	3	
95th Queue (ft)	18	
Link Distance (ft)		
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Movement	SB
Directions Served	LR
Maximum Queue (ft)	31
Average Queue (ft)	16
95th Queue (ft)	41
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Movement	EB	SB
Directions Served	LT	LR
Maximum Queue (ft)	4	50
Average Queue (ft)	0	26
95th Queue (ft)	3	49
Link Distance (ft)	4732	
Upstream Blk Time (%)		
Queuing Penalty (veh)		an are an internal and
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Movement	EB	SB
Directions Served	LT	LR
Maximum Queue (ft)	5	31
Average Queue (ft)	0	10
95th Queue (ft)	3	33
Link Distance (ft)	4732	
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Movement	SB
Directions Served	LR
Maximum Queue (ft)	31
Average Queue (ft)	10
95th Queue (ft)	33
Link Distance (ft)	
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Queuing and Blocking Report

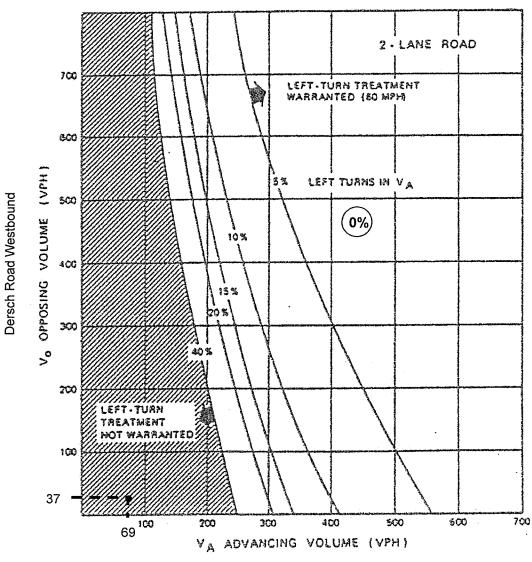
Cumulative + Project Weekday PM Pk. Hr.

Intersection: 1: Dersch Road & Leopard Drive

Movement	EB	SB
Directions Served	LT	LR
Maximum Queue (ft)	24	40
Average Queue (ft)	1	18
95th Queue (ft)	11	44
Link Distance (ft)	4732	
Upstream Blk Time (%)		
Queuing Penalty (veh)		AND AND DESCRIPTION OF
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 1: Dersch Road & Leopard Drive

Movement	EB	SB
Directions Served	LT	LR
Maximum Queue (ft)	10	62
Average Queue (ft)	0	29
95th Queue (ft)	5	53
Link Distance (ft)	4732	
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		



Dersch Road Eastbound

High Plains Shooting Range Project

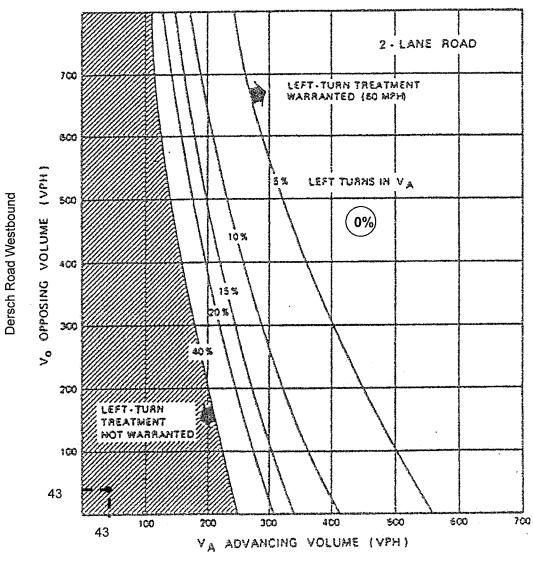
Dersch Road / Leopard Drive Intersection

EXISTING WEEKDAY PM PEAK HOUR

$$V_{A} = 69$$

L.T.
$$\% = 0/69 = 0\%$$

$$V_0 = 37$$



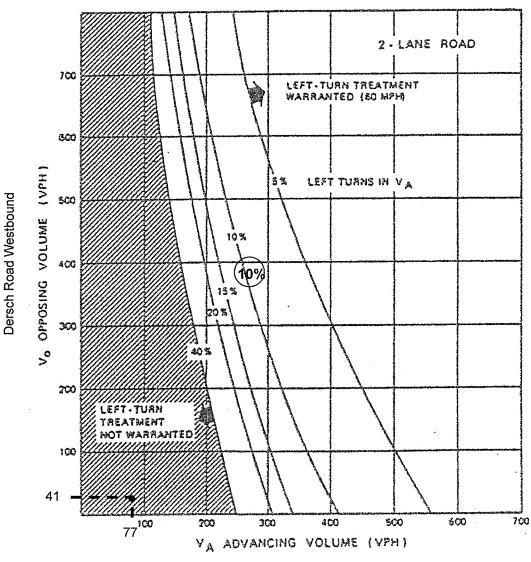
Dersch Road Eastbound

High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

EXISTING WEEKEND PEAK HOUR

$$V_A = 43$$
 L.T. % = 0/43 = 0% $V_O = 43$



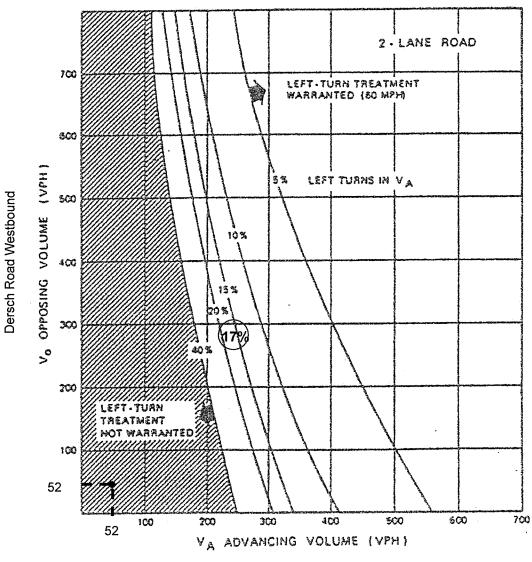
Dersch Road Eastbound

High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

EXISTING + PROJECT WEEKDAY PM PEAK HOUR

$$V_A = 77$$
 L.T. % = 8/77 = 10% $V_o = 4$



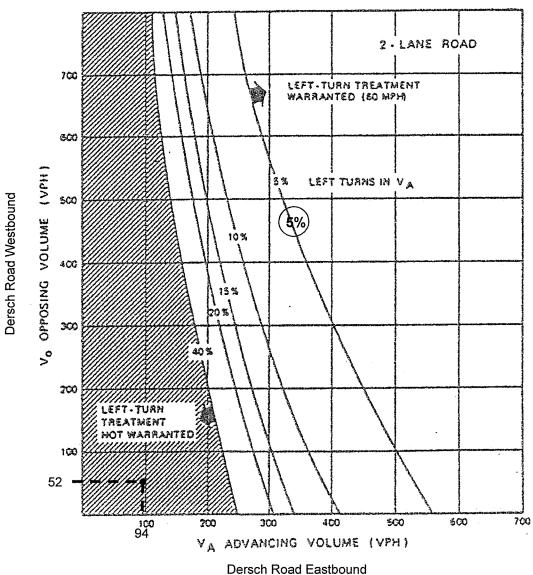
Dersch Road Eastbound

High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

EXISTING + PROJECT WEEKEND PEAK HOUR

$$V_A = 52$$
 L.T. % = 9/52 = 17% $V_O = 52$



Deisch Noad Lastbound

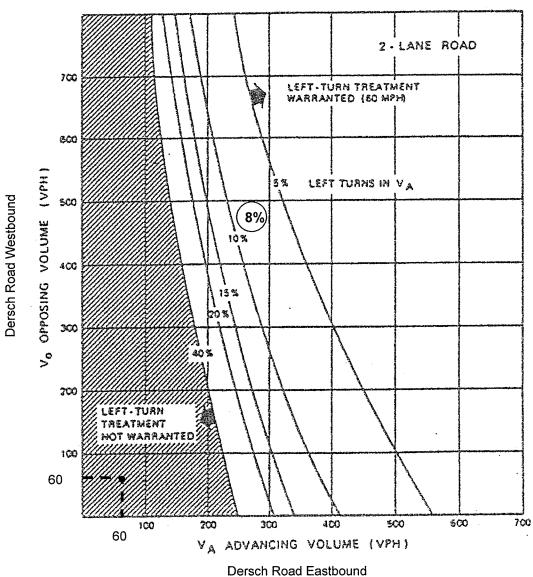
High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

CUMULATIVE YEAR 2035 WEEKDAY PM PEAK HOUR

$$V_{A} = 94$$

$$V_0 = 52$$



High Plains Shooting Range Project

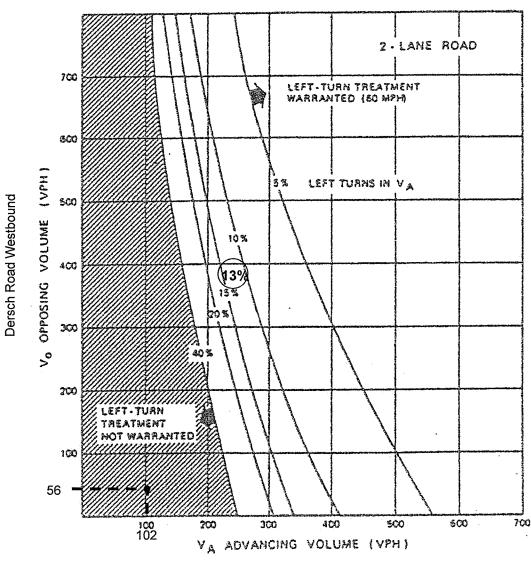
Dersch Road / Leopard Drive Intersection

CUMULATIVE YEAR 2035 WEEKEND PEAK HOUR

$$V_{A} = 60$$

L.T.
$$\% = 5/55 = 8\%$$

$$V_0 = 60$$



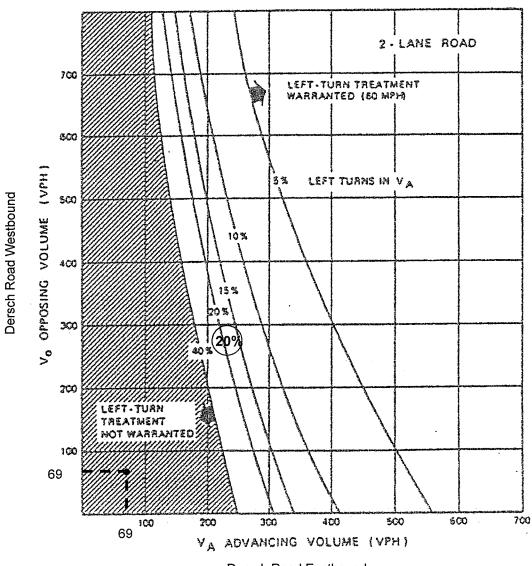
Dersch Road Eastbound

High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

CUMULATIVE YEAR 2035 + PROJECT WEEKDAY PM PEAK HOUR

$$V_A = 102$$
 L.T. % = 13/102 = 13% $V_o = 56$



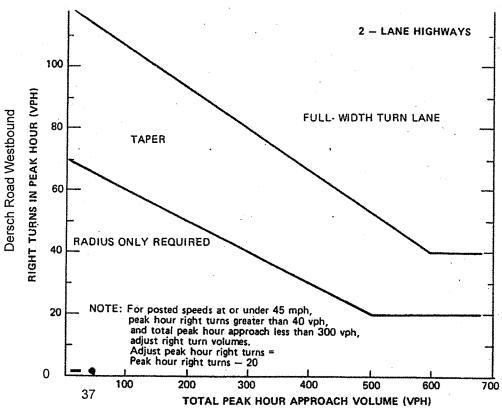
Dersch Road Eastbound

High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

CUMULATIVE YEAR 2035 + PROJECT WEEKEND PEAK HOUR

$$V_A = 69$$
 L.T. % = 14/69 = 20% $V_o = 69$

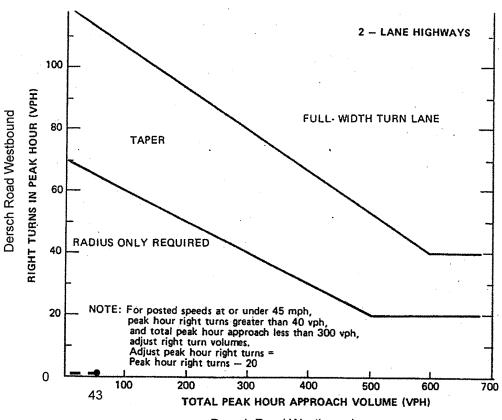


Dersch Road Westbound

High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

EXISTING WEEKDAY PM PEAK HOUR

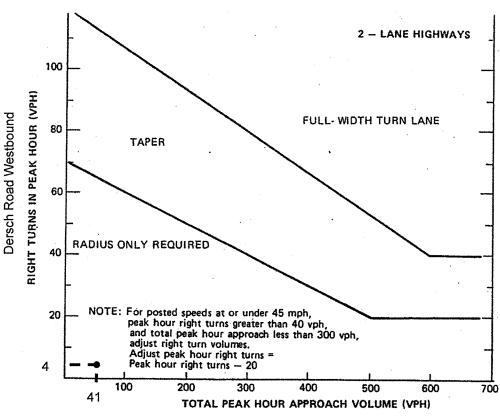


Dersch Road Westbound

High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

EXISTING WEEKEND PEAK HOUR

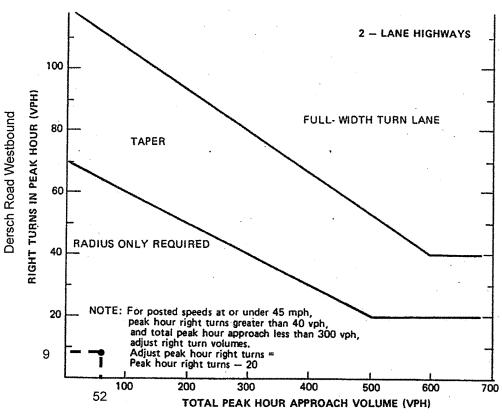


Dersch Road Westbound

High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

EXISTING + PROJECT WEEKDAY PM PEAK HOUR

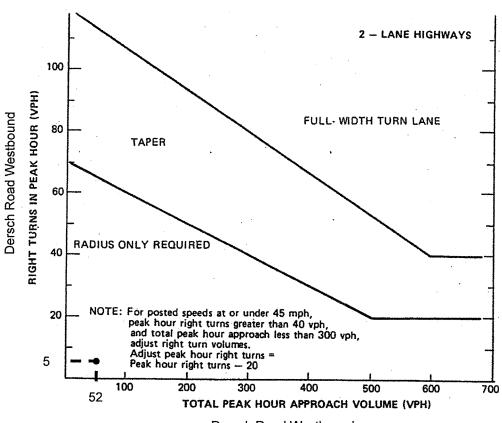


Dersch Road Westbound

High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

EXISTING + PROJECT WEEKEND PEAK HOUR

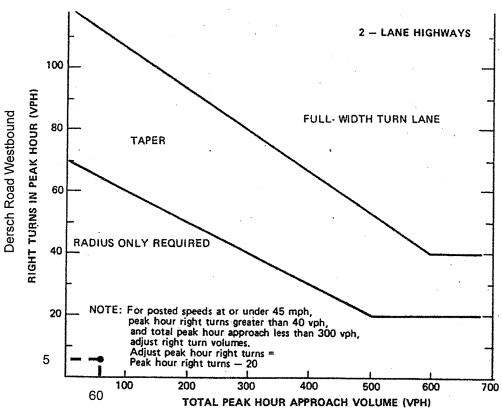


Dersch Road Westbound

High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

CUMULATIVE YEAR 2035 WEEKDAY PM PEAK HOUR

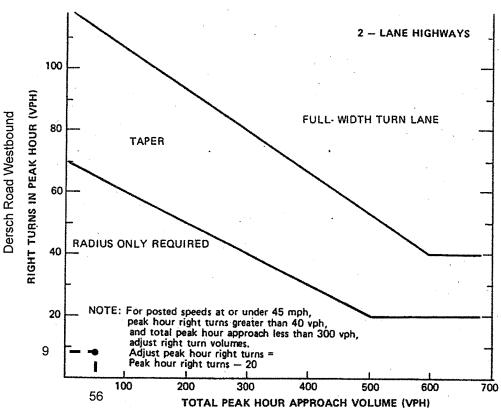


Dersch Road Westbound

High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

CUMULATIVE YEAR 2035 WEEKEND PEAK HOUR

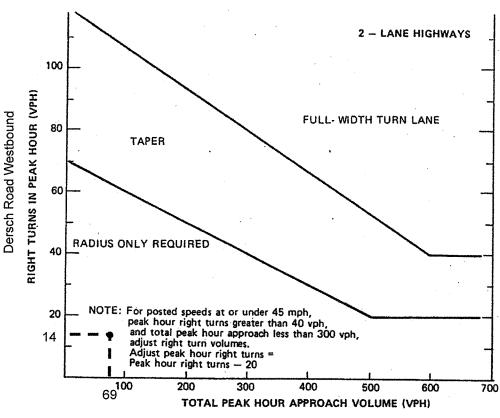


Dersch Road Westbound

High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

CUMULATIVE YEAR 2035 + PROJECT WEEKDAY PM PEAK HOUR



Dersch Road Westbound

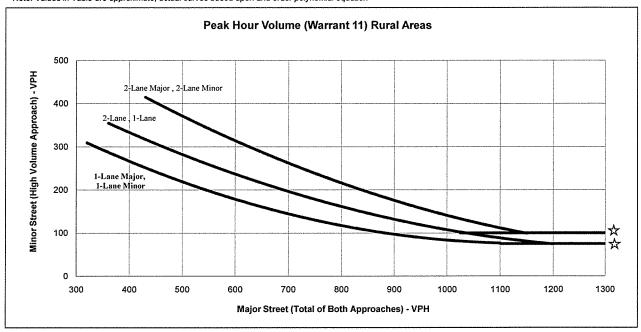
High Plains Shooting Range Project

Dersch Road / Leopard Drive Intersection

CUMULATIVE YEAR 2035 + PROJECT WEEKEND PEAK HOUR

Both 1 Lane Approaches		2 or more Lane and O	ne Lane Approaches	Both 2 or more Lane Approaches	
Major Street Total of	Minor Street High	Major Street Total of	Minor Street High	Major Street Total of	Minor Street High
Both Approaches	Volume Approach	Both Approaches	Volume Approach	Both Approaches	Volume Approach
370	280				
400	270	460	297	430	410
500	215	500	290	500	380
600	185	600	230	600	310
700	140	700	198	700	265
800	115	800	170	800	210
900	99	900	125	900	180
1000	85	1000	105	1000	140
1100	75	1100	90	1100	110
1200	. 75	1200	75	1150	100
1300	75	1300	75	1300	100

^{*} Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation



100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:

Dersch Road / Leopard Drive

Scenario: Minor St. Volume:

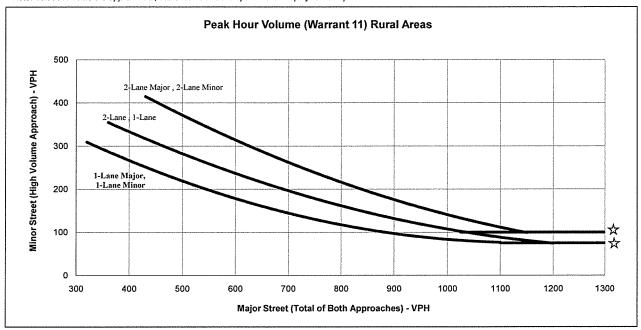
Existing Weekday PM Peak Hour Conditions

Major St. Volume:

Warrant Met?:

Both 1 Lane Approaches		2 or more Lane and O	ne Lane Approaches	Both 2 or more Lane Approaches	
Major Street Total of	Minor Street High	Major Street Total of	Minor Street High	Major Street Total of	Minor Street High
Both Approaches	Volume Approach	Both Approaches	Volume Approach	Both Approaches	Volume Approach
370	280				
400	270	460	297	430	410
500	215	500	290	500	380
600	185	600	230	600	310
700	140	700	198	700	265
800	115	800	170	800	210
900	99	900	125	900	180
1000	85	1000	105	1000	140
1100	75	1100	90	1100	110
1200	75	1200	75	1150	100
1300	75	1300	75	1300	100

^{*} Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation



$\stackrel{\star}{\sim}$

NOTE:

100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:

Dersch Road / Leopard Drive

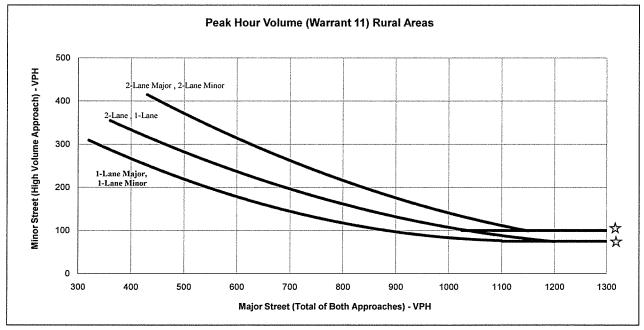
Scenario: Minor St. Volume:

Existing Weekend Peak Hour Conditions

Minor St. Volume: Major St. Volume: Warrant Met?:

Both 1 Lane Approaches		2 or more Lane and O	ne Lane Approaches	Both 2 or more Lane Approaches	
Major Street Total of	Minor Street High	Major Street Total of	Minor Street High	Major Street Total of	Minor Street High
Both Approaches	Volume Approach	Both Approaches	Volume Approach	Both Approaches	Volume Approach
370	280				
400	270	460	297	430	410
500	215	500	290	500	380
600	185	600	230	600	310
700	140	700	198	700	265
800	115	800	170	800	210
900	99	900	125	900	180
1000	85	1000	105	1000	140
1100	75	1100	90	1100	110
1200	75	1200	75	1150	100
1300	75	1300	75	1300	100

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100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:

Dersch Road / Leopard Drive

Scenario:

Existing + Project Weekday PM Peak Hour Conditions

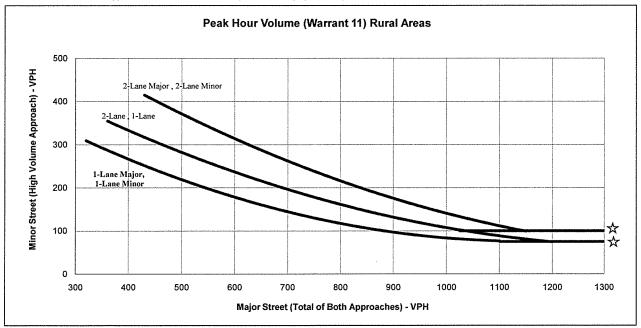
Minor St. Volume: Major St. Volume:

118

Warrant Met?:

Both 1 Lane	Both 1 Lane Approaches		2 or more Lane and One Lane Approaches		ane Approaches
Major Street Total of	Minor Street High	Major Street Total of	Minor Street High	Major Street Total of	Minor Street High
Both Approaches	Volume Approach	Both Approaches	Volume Approach	Both Approaches	Volume Approach
370	280				
400	270	460	297	430	410
500	215	500	290	500	380
600	185	600	230	600	310
700	140	700	198	700	265
800	115	800	170	800	210
900	99	900	125	900	180
1000	85	1000	105	1000	140
1100	75	1100	90	1100	110
1200	75	1200	75	1150	100
1300	75	1300	75	1300	100

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100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:

Dersch Road / Leopard Drive

Scenario:

Existing + Project Weekend Peak Hour Conditions

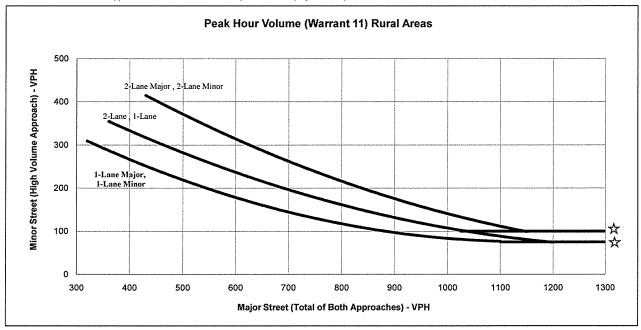
Minor St. Volume:

42

Major St. Volume: Warrant Met?:

Both 1 Lane Approaches		2 or more Lane and One Lane Approaches		Both 2 or more Lane Approaches	
Major Street Total of	Minor Street High	Major Street Total of	Minor Street High	Major Street Total of	Minor Street High
Both Approaches	Volume Approach	Both Approaches	Volume Approach	Both Approaches	Volume Approach
370	280				
400	270	460	297	430	410
500	215	500	290	500	380
600	185	600	230	600	310
700	140	700	198	700	265
800	115	800	170	800	210
900	99	900	125	900	180
1000	85	1000	105	1000	140
1100	75	1100	90	1100	110
1200	75	1200	75	1150	100
1300	75	1300	75	1300	100

^{*} Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation



NOTE:

100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:

Dersch Road / Leopard Drive

Scenario: Minor St. Volume: Cumulative Year 2035 Weekday PM Peak Hour Conditions

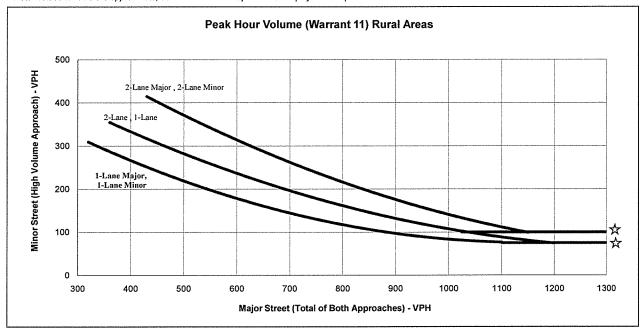
Major St. Volume:

10 146

Warrant Met?:

Both 1 Lane	Both 1 Lane Approaches		ne Lane Approaches	Both 2 or more Lane Approaches	
Major Street Total of	Minor Street High	Major Street Total of	Minor Street High	Major Street Total of	Minor Street High
Both Approaches	Volume Approach	Both Approaches	Volume Approach	Both Approaches	Volume Approach
370	280				
400	270	460	297	430	410
500	215	500	290	500	380
600	185	600	230	600	310
700	140	700	198	700	265
800	115	800	170	800	210
900	99	900	125	900	180
1000	85	1000	105	1000	140
1100	75	1100	90	1100	110
1200	75	1200	75	1150	100
1300	75	1300	75	1300	100

^{*} Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation



NOTE: 100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:

Dersch Road / Leopard Drive

Scenario:

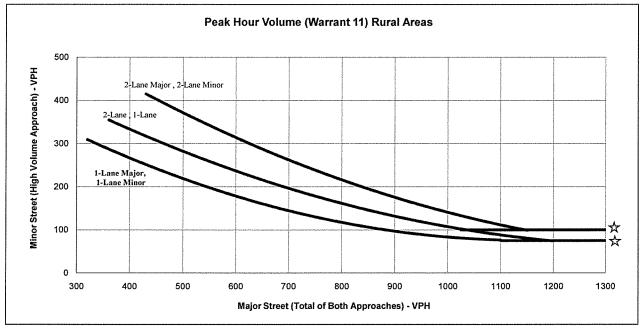
Cumulative Year 2035 Weekend Peak Hour Conditions

Minor St. Volume: Major St. Volume: 10 120

Warrant Met?:

Both 1 Lane Approaches		2 or more Lane and C	ne Lane Approaches	Both 2 or more Lane Approaches	
Major Street Total of	Minor Street High	Major Street Total of	Minor Street High	Major Street Total of	Minor Street High
Both Approaches	Volume Approach	Both Approaches	Volume Approach	Both Approaches	Volume Approach
370	280				
400	270	460	297	430	410
500	215	500	290	500	380
600	185	600	230	600	310
700	140	700	198	700	265
800	115	800	170	800	210
900	99	900	125	900	180
1000	85	1000	105	1000	140
1100	75	1100	90	1100	110
1200	75	1200	75	1150	100
1300	75	1300	75	1300	100

^{*}Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation



NOTE: 100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:

Dersch Road / Leopard Drive

Scenario:

Cumulative Year 2035 + Project Weekday PM Peak Hour Conditions

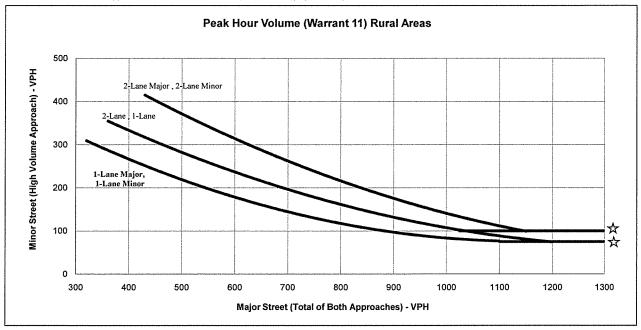
Minor St. Volume: Major St. Volume:

158

Warrant Met?:

Both 1 Lane Approaches		2 or more Lane and O	ne Lane Approaches	Both 2 or more Lane Approaches	
Major Street Total of	Minor Street High	Major Street Total of	Minor Street High	Major Street Total of	Minor Street High
Both Approaches	Volume Approach	Both Approaches	Volume Approach	Both Approaches	Volume Approach
370	280				
400	270	460	297	430	410
500	215	500	290	500	380
600	185	600	230	600	310
700	140	700	198	700	265
800	115	800	170	800	210
900	99	900	125	900	180
1000	85	1000	105	1000	140
1100	75	1100	90	1100	110
1200	75	1200	75	1150	100
1300	75	1300	75	1300	100

^{*} Note: Values in Table are approximate, actual curves based upon 2nd order polynomial equation



100 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR MINOR STREET APPROACH WITH TWO OR MORE LANES AND 75 VPH APPLIES AS THE LOWER THRESHOLD VOLUME FOR A MINOR STREET APPROACHING WITH ONE LANE.

Intersection:

Dersch Road / Leopard Drive

Scenario:

Cumulative Year 2035 + Project Weekend Peak Hour Conditions

Minor St. Volume: Major St. Volume:

138

Warrant Met?: